

**Electrical oscillations induced by the metal-insulator transition in VO<sub>2</sub>**Hyun-Tak Kim,<sup>1,a)</sup> Bong-Jun Kim,<sup>1</sup> Sungyoul Choi,<sup>1</sup> Byung-Gyu Chae,<sup>1</sup>  
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We systematically investigate the characteristics of an electrical oscillation observed in two-terminal vanadium dioxide (VO<sub>2</sub>) devices. These oscillations are observed at room temperature in a simple electrical circuit without inductive components. The circuit is composed only of a dc voltage source, the VO<sub>2</sub> device, and a standard resistor connected in series with the device. We explain why the observed oscillations are a result of the percolative metal-to-insulator transition (MIT) of VO<sub>2</sub> and the coexistence of the metal and insulating phases. Specifically, oscillations are attributed to the construction and destruction of capacitive regions composed of regions of the semiconducting phase, (as dielectric material) and metallic phase electron carriers, induced by the MIT (as capacitor electrodes). Since the coexistence of these phases—and thus the capacitive regions—is destroyed by elevated temperature, the MIT oscillation is not explained in terms of significant heat input but rather in terms of a voltage-triggered effect. It is also discussed whether the current jump at the onset of the oscillations is driven by Mott physics or by Peierls physics relying on a structural phase transition. Furthermore, the electrical parameter space surrounding these oscillations is explored, and a generation window is identified. Within this generation window, the oscillation frequency can be continuously tuned by adjusting applied voltage or by an external circuit component, such as resistor or added capacitor. The frequency of oscillations can be increased up to >1 MHz.

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**I. INTRODUCTION**

Mott<sup>1</sup> predicted in 1949 that a first-order discontinuous metal-insulator transition (MIT) could arise from the removal of electrons in a strongly correlated electron system (or Mott insulator). The critical driving parameter in this transition is the on-site repulsive Coulomb interaction  $U_C$ .<sup>2</sup> This concept has been derived by the extension of the Brinkman–Rice picture<sup>3,4</sup> and is based on inhomogeneity. The removal of electrons, regarded as doping of hole carriers, causes a breakdown of  $U_C$  in a Mott insulator with a hole concentration below 0.01% and induces the breakdown of an energy gap formed by  $U_C$  through impact ionization;<sup>5–7</sup> this is the hole-driven MIT generated at a critical hole concentration,  $n_c$ , not the metallic minimum carrier density in the Mott criterion.<sup>1,4</sup> In this case, both a metal phase with electron carriers and a semiconductive system with hole carriers can be formed. The metal phase has a strong correlation between electrons.<sup>2,8</sup> The semiconductive system is a remnant component of the parent Mott insulator which is an extrinsic compound semiconductor with disorder, impurities, dislocation, etc. The Mott system (or insulator) has two kinds of carriers<sup>4,9</sup> and is intrinsically inhomogeneous.<sup>10,11</sup>

In strongly correlated system, there are several explanations besides Mott's first-order theory: a Hubbard MIT,<sup>12</sup> which undergoes a continuous transition from metal to insulator following the increase in  $U$ , and a Peierls continuous

MIT<sup>13</sup> driven by electron-phonon interactions, such as charge density wave (CDW), which induce a structural phase transition (SPT).<sup>14</sup>

In the context of the above MIT theories, VO<sub>2</sub> ( $3d^1$ ) is a very interesting material because it is a representative insulator with both an energy gap of 0.6 eV and the metallic electronic structure of half filling. It undergoes a large resistance change (regarded as the MIT) near critical temperature  $T_C \approx 67$  °C and a SPT between the monoclinic structure (below  $T_C$ ) and the tetragonal rutile structure above  $T_C$ .<sup>15</sup>

The insulator structure of VO<sub>2</sub> was known as the monoclinic one,  $M_1$ , at enough low temperatures compared to  $T_C$  and at room temperature. With increasing temperature,  $M_1$  changed to  $M_2$  just below  $T_C$  via an intermediate triclinic monoclinic structure T, and finally was transformed to the rutile R tetragonal structure of the metallic phase above  $T_C$ .<sup>16</sup>  $M_2$  is composed of two distorted structures; one-half of the V chain pairs but does not twist (this forms charge ordering of CDW) and the other half twists but does not pair (this is an equally spaced V zigzag chain and forms the Mott–Hubbard insulator).<sup>17,18</sup>  $M_1$  is defined by a superposition of two distorted structures in  $M_2$ .<sup>17,18</sup> For  $V_{1-x}Cr_xO_2$ , with doping concentration  $x$ , the  $M_1$  structure of the insulator phase at room temperature was transformed into  $M_2$  via  $M_3$ .<sup>17</sup> Moreover, for VO<sub>2</sub> nanorods with the semiconducting characteristic below and over 190 K, a small jump in conductivity and photocurrent decay near 190 K was interpreted as a first-order SPT between  $M_2$  and T structures.<sup>19</sup>

Researches on the MIT of VO<sub>2</sub> have mainly focused on the mechanism responsible for the SPT between the mono-

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clinic insulating phase and the tetragonal rutile metal phase.<sup>20–24</sup> However, Kim *et al.*<sup>5,8</sup> concentrated researches on the presence of a resistivity change as MIT, which is not accompanied by any SPT, and the observation of a strong correlation. The presence of a MIT independent of any SPT (a metal phase with the monoclinic structure) was experimentally observed by several experiments such as Raman scattering with temperature,<sup>25</sup> Raman-scattering under high pressure,<sup>26–28</sup> infrared transmission and reflectivity for  $V_{1-x}Cr_xO_2$  under high pressure,<sup>29</sup> careful study of coherent phonons,<sup>30</sup> micro-X-ray diffraction,<sup>31</sup> programmable critical-temperature sensor,<sup>32</sup> strain-induced MIT in single-domain nanobeam,<sup>33</sup> and electron diffraction.<sup>34</sup> Wei *et al.*<sup>33</sup> showed a metal phase in the coexistence regime in nanobeams below a temperature where a kink occurs between the supercooled and stable metallic phases. Since the kink is similar to a kink of the SPT measured at  $I$ - $V$  curves,<sup>31</sup> the kink can be regarded as the SPT. Then the metallic phase below the kink temperature can be interpreted as the metal phase with a monoclinic structure. Moreover, the metal phase with a monoclinic structure for a  $V_{1-x}Mo_xO_2$  ceramic sample was also observed by a nanolevel x-ray diffraction experiment.<sup>35</sup> Gopalakrishnan *et al.*<sup>36</sup> revealed that MIT is independent of the SPT through simulations based on the thermal model. The divergent effective mass in the metal phase as evidence of strong correlations was analyzed via using effective medium theory to determine optical parameters within true nanoscale grain regions in a heterogeneous system.<sup>8</sup> Hole charges below  $T_C \approx 67$  °C were observed by Hall effect measurement.<sup>5,9</sup> The electrostatic method also revealed the presence of hole charges in  $VO_2$ .<sup>37</sup> The Mott–Hubbard bands were directly observed by resonance of  $3d^0 + 3d^1L$  and  $3d^1C$  states by  $V$   $2p$ - $3d$  resonant photoemission spectroscopy<sup>38</sup> and broadness of  $\pi$  band including  $d_{11}$  band.<sup>39</sup>

The summation of the above investigations is overwhelming evidence supporting a hole-driven Mott MIT. However, the issue is yet to be completely settled, due to some evidence in favor of Peierls MIT, such as observation of the tetragonal phonon at 6 THz<sup>40</sup> and a rapid decrease in transmission<sup>41</sup> observed by the femtosecond technique. Thus, it has been long debated whether this MIT in  $VO_2$  is driven by Mott or Peierls physics.<sup>18,42</sup>

The voltage-induced current jump observed in experiments,<sup>5,43</sup> regarded as the MIT, is not generated by temperature increase and thus is evidence for a hole-driven MIT. This electrical jump has attracted interest of great many researchers because an abrupt resistance switching mediated by voltage-induced MIT can give versatile practical applications.<sup>5,43</sup>

The diverging MIT instabilities<sup>3,4</sup> for a strongly correlated system could predict such an electrical oscillation in a serial circuit composed of a resistance and a MIT device.<sup>44</sup> Observations of the MIT electrical oscillation in  $VO_2$  were previously reported.<sup>45,46</sup> This oscillation generated by the voltage-induced MIT can be evidence to support the hole-driven Mott MIT model because such high-frequency

oscillations are unlikely to exist within a thermally driven SPT Peierls system. The thermal timescales, as well as the known hysteretic behavior of the SPT when switching between monoclinic and tetragonal structures occurs, prohibit such high-frequency oscillations.

In earlier studies, electrical oscillations similar to those we observed, but with a sinusoidal waveform, were observed in GaAs,<sup>47</sup>  $K_{0.3}MoO_3$ ,<sup>48</sup> and  $\theta$ -(BEDT-TTF)<sub>2</sub>CsCo(SCN)<sub>4</sub>.<sup>49,50</sup> The Gunn oscillation in GaAs was explained in terms of the negative differential resistance (NDR) caused by mobility change from (100) to (110).<sup>51</sup> The NDR characteristic is similar to the thyristor one.<sup>52</sup> For  $K_{0.3}MoO_3$ , the sliding motion of the CDW undergoing the SPT was suggested as the oscillation mechanism, and the oscillation frequency  $f_{osc}$  could be changed from 10 to 17 kHz by varying the applied voltage at 17 K.<sup>48</sup> The 40 Hz oscillation in  $\theta$ -(BEDT-TTF)<sub>2</sub>CsCo(SCN)<sub>4</sub> was also observed at 4.2 K.<sup>49</sup> The current jump in the organic material was explained by melting of charge ordering with a charge difference between nearest neighbors. The charge difference is regarded as the CDW. The melting of the charge ordering is similar to the sliding of the CDW in  $K_{0.3}MoO_3$  and indicates the melting of the structure distorted by electron-phonon interaction. This analysis is acceptable for organic and CDW materials. However, as far as a correlated material such as  $VO_2$ , the mechanism of the oscillation is different from that in CDW materials. The physical reasons for these differences will be discussed in Sec. IV.

In this paper, we investigate the characteristics of a high-frequency room-temperature electrical oscillation observed in the  $VO_2$ -based two-terminal devices with S-type NDR characteristics. We demonstrate the generation mechanism of this oscillation by analyzing experimental data based on inhomogeneity. We show that increasing applied source voltage to the device causes percolation and increases the oscillation frequency  $f_{osc}$  by effectively decreasing the device capacitance.

Values for the capacitance of the device are found by fitting exponential charging curves. Furthermore, an overall generation window for the MIT oscillation is found in terms of the external resistance and source voltage. In particular, the effect of the external circuit components, such as a voltage source, resistor, and capacitor, on  $f_{osc}$  is systematically investigated. Thus, we reveal that  $f_{osc}$  can be designed to be increased up to >1 MHz and controlled by simple adjustment of some external circuit components.

## II. EXPERIMENTS

In order to fabricate the two-terminal  $VO_2$  device shown in Fig. 1(a),  $VO_2$  thin films were grown on sapphire ( $Al_2O_3$ ) substrates by employing a sol-gel method.<sup>53</sup> Note that  $VO_2$  films could be deposited by several deposition methods.<sup>54</sup> The films were patterned into a line shape to make a current channel with photolithography processes and a rf ion-beam milling technique. A Ni electrode layer was deposited on the etched  $VO_2$  layer using a rf magnetron sputter deposition

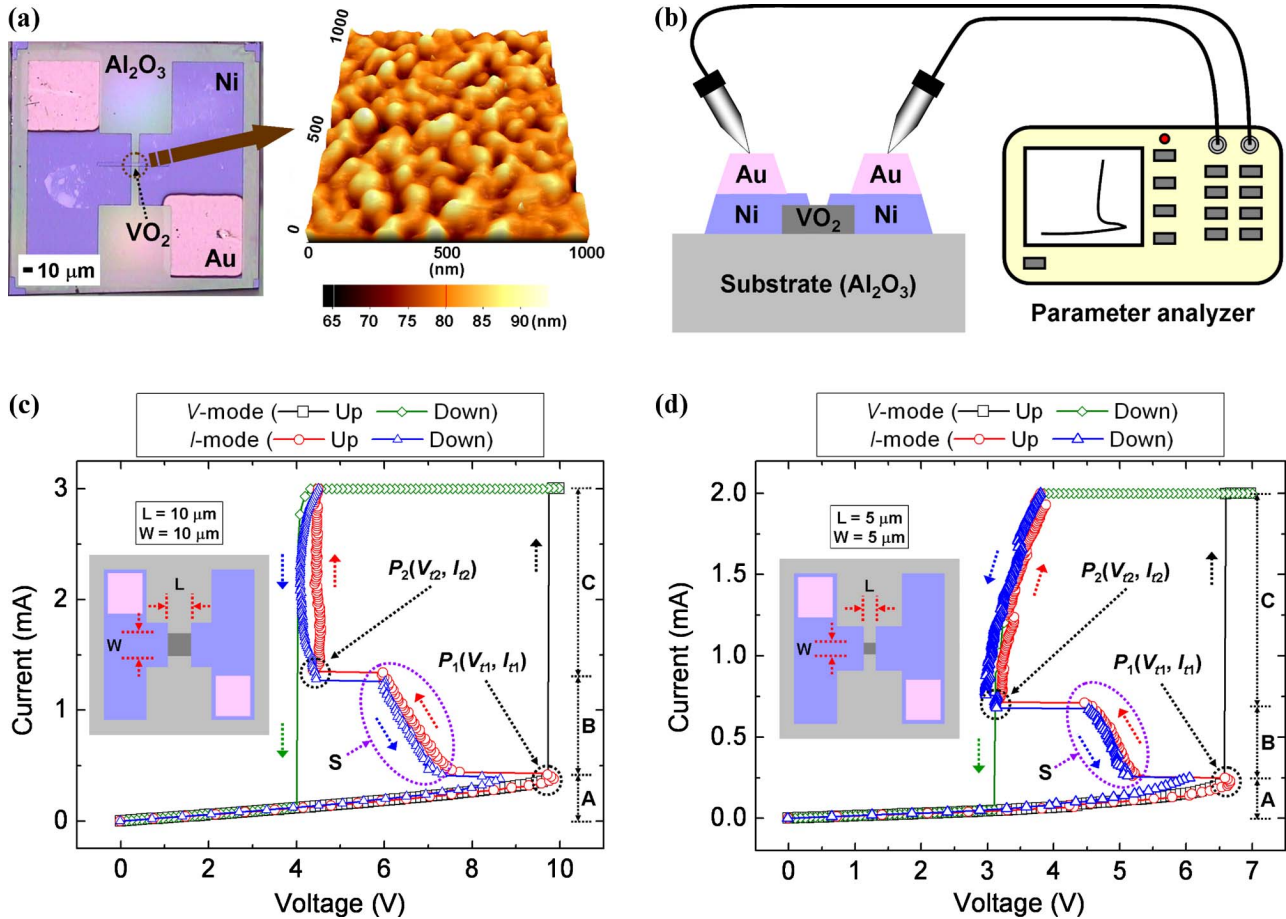


FIG. 1. (Color online) (a) Optical microscope plane-view image of a VO<sub>2</sub>-based two-terminal device and the surface morphology of the VO<sub>2</sub> film used in the device. (b) Schematic diagram of the experimental setup to measure  $I$ - $V$  characteristics of the device. Measured  $I$ - $V$  hysteresis characteristics of (c) device I ( $10 \times 10 \mu\text{m}^2$ ) and (d) device II ( $5 \times 5 \mu\text{m}^2$ ).

technique and was patterned with a lift-off method. For direct microcontact electrical measurements, square-shape gold electrodes of  $50 \times 50 \mu\text{m}^2$  were patterned on Ni electrodes of the device. The width of the VO<sub>2</sub> patch was designed to be narrower than that of the electrodes to avoid any delayed transition of VO<sub>2</sub> outside the electrodes. The final dimensions of the exposed film patches in the fabricated devices were  $10 \times 10 \mu\text{m}^2$  (device I) and  $5 \times 5 \mu\text{m}^2$  (device II). The thickness of the VO<sub>2</sub> films was approximately 100 nm.

The schematic diagram of the experimental setup to measure  $I$ - $V$  characteristics of the device is shown in Fig. 1(b). For the  $I$ - $V$  measurements, we used a microprobe station (Micromanipulator) with tungsten probes ( $5 \mu\text{m}$  in diameter) and a parameter analyzer (Agilent B1500A). The Ohmic contact resistance of the devices was below  $1 \Omega$ , which is negligible compared with the device resistance  $R_D$  at room temperature. The  $I$ - $V$  characteristics of the devices were obtained by using the  $V$ -mode and  $I$ -mode of the parameter analyzer. The  $V$ -mode and  $I$ -mode are the measurement modes to detect the current and voltage across the device,  $I_D$  and  $V_D$ , as a function of the applied voltage ( $V$ -mode) and current ( $I$ -mode), respectively. Moreover, the stability of the MIT current-jump threshold point, responsible for the observed switching, was confirmed.<sup>55</sup>

### III. MEASUREMENT OF MIT ELECTRICAL OSCILLATION

#### A. Oscillation measurement and investigation of its generation mechanism

Figure 1(a) shows an optical microscope plane-view image of the fabricated two-terminal VO<sub>2</sub> device (device I) and the surface morphology of the VO<sub>2</sub> film used in the device (a rms roughness of  $\sim 5 \text{ nm}$ ). The film surface was comprised of grains of several different sizes. At room temperature, the VO<sub>2</sub> film has almost insulating VO<sub>2</sub> grains (high resistance dielectric components). At a critical temperature ( $\sim 340 \text{ K}$ ), high resistance insulating grains begin to turn into low resistance metallic ones, and most insulating grains have transitioned into metallic ones just after the critical temperature.<sup>27,28</sup> Any void between grains (which will have large resistance) and non-VO<sub>2</sub> phases in the film such as V<sub>2</sub>O<sub>5</sub> can affect  $R_D$  throughout the entire process of the voltage-induced MIT.<sup>23</sup> Recently, it was observed that the MIT begins percolation near grain boundaries or void regions, suggesting that these have a strong role in the MIT transition dynamics.<sup>11</sup>

Figures 1(c) and 1(d) show the  $I$ - $V$  hysteresis loops measured at room temperature for device I and device II, respectively. Below the threshold of any current-jumps [in region A of Figs. 1(c) and 1(d)], device I and device II exhibit semi-

conducting behavior with hole charges.<sup>4,9</sup> There exist two threshold instability voltages ( $V_{t1}, V_{t2}$ ) where abrupt current changes happen. At  $V_{t1}$ , a critical carrier density inducing the jump,  $n_c$ , is reached.<sup>4</sup> In  $V$ -mode traces, ( $V_{t1} \approx 9.7$  V,  $V_{t2} \approx 4.0$  V) in device I and (6.6 V, 3.1 V) in device II were measured. The currents at  $V_{t1}$  and  $V_{t2}$  are designated as  $I_{t1}$  and  $I_{t2}$ , respectively. The  $V$ -mode traces have large hysteresis loops with black and green jumps corresponding to negative and positive jumps in resistance, respectively. In the  $I$ -mode traces of both Figs. 1(c) and 1(d), a typical feature of the S-type NDR is shown between instability  $P_1(V_{t1}, I_{t1})$  and instability  $P_2(V_{t2}, I_{t2})$ . The NDR behavior arises from the restriction of current and has little hysteresis width. This indicates that  $I$ -mode generates little heat and no SPT. Anomalous behavior—decreasing voltage with increasing current—was observed in a semiconductor phase between instabilities  $P_1$  and  $P_2$  (S section in region B). This behavior indicates that the MIT occurs gradually, resulting in a gradual decrease in resistance (gradual increase in electrical conductivity). This observation is interpreted as evidence for a percolative transition<sup>8,28,56</sup> and is evidence of inhomogeneity in the VO<sub>2</sub> film. It is also observed by comparing device I with device II that the increase in the device dimension causes both threshold voltages and corresponding currents to increase and thus the NDR region to expand as well. Despite the dimension change, however, no noticeable variation was observed in the differential resistance ( $dV/dI$ ), estimated as approximately  $-500 \Omega$  from the measurement results. Furthermore, the oscillation is affected by external parameters such as a kind of electrodes, lattice-film mismatch, and film thickness. When electrical characteristics of a device are changed by the external parameters, current near zero voltage (leakage current),  $V_{t1}$ , and  $I_{t2}$  vary,<sup>5</sup> for example, a large contact resistance between film and a metal electrode with a low conductivity, a large lattice-substrate mismatch, and a more thick film induce a large leakage current, a reduced  $V_{t1}$ , and an increased  $I_{t2}$ .

Moving on to the experiments involving electrical oscillation, Fig. 2(a) shows a schematic diagram of the electrical circuit used for generating the MIT oscillation and controlling  $f_{osc}$ . The single-loop circuit was composed of a VO<sub>2</sub> device (device I or device II), a voltage source of a dc voltage  $V_S$ , and an external resistor of a resistance  $R_E$ . In order to reduce the generation of an excess Joule heat, both a function generator (Agilent 33120A) and a dc power supply were used for generating rectangular voltage pulses with a variety of dc offsets. The oscillatory electrical responses were recorded by a digital oscilloscope (HP 54810A). An external capacitor of a capacitance  $C_E$  in the dashed box can also be connected in parallel to the external resistor giving further control of  $f_{osc}$ . In fact, all circuit parameters ( $V_S$ ,  $R_E$ , and  $C_E$ ) can act as frequency tuning controls, and related experimental results are provided in Figs. 4 and 5.

Figure 2(b) shows the oscillatory electrical traces of  $V_D$  (blue diamonds) and  $I_D$  (red circles) measured with device I at room temperature, when a single voltage pulse with a peak value of  $V_S$  ( $V_S^p$ ) of 13.8 V (including a dc offset of 10 V) and a pulse width of 25  $\mu$ s is applied ( $R_E=8$  k $\Omega$ ). The voltage across the external resistor  $V_E$  is directly measured, and  $V_D$

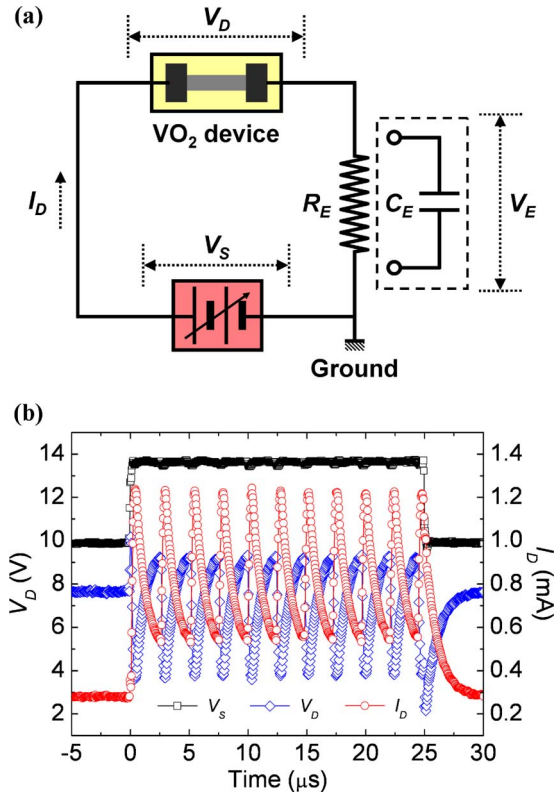


FIG. 2. (Color online) (a) Schematic diagram of the electrical circuit used for the generation of the MIT electrical oscillation. In order to control  $f_{osc}$ , an external capacitor in a dashed box can be employed and connected to an external resistor in parallel. (b) Electrical waveforms of  $V_D$  (blue diamonds) and  $I_D$  (red circles) measured at room temperature when a voltage pulse with  $V_S^p=13.8$  V (including a dc offset of 10 V) and a pulse width of 25  $\mu$ s are applied ( $R_E=8$  k $\Omega$ ).

and  $I_D$  are obtained by  $(V_S - V_E)$  and  $(V_E/R_E)$ , respectively. The peak-to-peak amplitudes of the oscillation waveforms of  $V_D$  and  $I_D$  were measured as  $\sim 5.7$  V and  $\sim 0.7$  mA, respectively. The fundamental component of  $f_{osc}$  was measured as  $\sim 0.525$  MHz. Note that a device without the NDR shown in region B of Figs. 1(c) and 1(d) did not generate any oscillation.

Considering one period of the oscillation in Fig. 2(b), the exponential buildup and decay of  $V_D$  and  $I_D$ , respectively, are driven by the carrier charging process in a series RC circuit—whose electrical response time is restricted by a capacitive time constant  $\tau_0$  given by  $R_E C_D$  where  $C_D$  is a device capacitance. Within one period of the oscillation, the charging curve responses of  $V_D$  and  $I_D$ , before the MIT threshold jump is triggered, can be fitted by the following expressions derived based on the RC circuit analysis;

$$V_D(t) \propto V_S^p [1 - \exp(-t/\tau_0)], \quad (1)$$

$$I_D(t) \propto V_S^p [1 + (R_D/R_E) \exp(-t/\tau_0)]. \quad (2)$$

The overall picture of the oscillations can be understood as follows: in region A of Figs. 1(c) and 1(d), insulating VO<sub>2</sub> grains (high resistance dielectric components with hole charges) constitute most of the VO<sub>2</sub> film. At  $V_D=V_{t1}$ , an abrupt current jump (MIT) occurs, and an abrupt decrease in  $R_D$  takes place. Here insulating grains begin to turn into me-

tallic ones, and metallic electron carriers appear (region B); a capacitor is formed, which consists of a dielectric semiconducting component (S in region B) and the electron carriers. In conjunction with the swift decrease in  $R_D$ ,  $V_D$  instantaneously drops down below  $V_{I2}$ , and  $I_D$  rapidly increases. Then,  $V_D$  is restored to  $V_{I2}$  by some repulsive force—designated as the elastic restoring force by Sakai.<sup>46</sup> Behavior of  $V_D$  after this moment is determined by  $I_D$  affected directly by  $R_D$  and  $R_E$ .

When we select an appropriate  $R_E$  that forces  $I_D < I_{I2}$ , the device can return to its insulating state. The cycle can repeat with  $V_D$  increasing again. In this condition, the temporal buildup of  $V_D$  [Eq. (1)] proceeds to occur until  $V_D$  reaches  $V_{I1}$ . After  $V_D$  reaches  $V_{I1}$ , the MIT jump occurs, rapidly discharging  $V_D$ , and the same process described above repeats as long as  $V_S^p$  is large enough to make  $V_D$  become  $V_{I1}$ . In this manner, the MIT oscillation is maintained between both instabilities  $P_1(V_{I1}, I_{I1})$  and  $P_2(V_{I2}, I_{I2})$ , as indicated in Figs. 1(c) and 1(d).

In the case of  $R_E$  selected such that  $I_D > I_{I2}$ , just after the MIT [region C of Figs. 1(c) and 1(d)], most insulating VO<sub>2</sub> grains have become metallic ones, and the film has few dielectric regions. The decreased dielectric (capacitive) component of the film causes a reduced number of charges to build on the VO<sub>2</sub> device and prevents  $V_D$  from increasing to  $V_{I1}$  again. In other words, the disappearance of the capacitive component of the film makes it impossible for the VO<sub>2</sub> device to recover its insulating state (high resistance state) and perform oscillations.

## B. Nanoscale percolation: Explanation of forming capacitor

An explanation on the presence and absence of the capacitive component in the VO<sub>2</sub> device after the MIT ( $V_D > V_{I1}$ ) is now given, as shown in Fig. 3(a). A VO<sub>2</sub> film composed of many grains [Fig. 1(a)] can be thought of as being comprised of two components: any VO<sub>2</sub> phase (green or red grains) and any non-VO<sub>2</sub> material such as vacuum or V<sub>2</sub>O<sub>5</sub> (gray bottom). The amount of the non-VO<sub>2</sub> phase may be negligible in a high-quality film. Looking only at the VO<sub>2</sub> material, when  $V_D < V_{I1}$  [plot I of Fig. 3(a)], the film is fully filled with green grains (insulating state) without red grains (metallic state). When  $V_D$  starts to exceed  $V_{I1}$  [plot II of Fig. 3(a)], one part of the VO<sub>2</sub> phase turns into a metallic state, and the other part still remains an insulating state due to the minute compositional inhomogeneity between VO<sub>2</sub> grains. Green and red grains may act as dielectric components and metal electrodes, respectively. Averaged across the entire film, they build a capacitor across the device. This intermediate state corresponds to the region B in Figs. 1(c) and 1(d). When  $I_D$  exceeds  $I_{I2}$ , the film is occupied with primarily red grains resulting in vanishing capacitive component of the device [plot III of Fig. 3(a)].

This simple explanation is supported by midinfrared near-field images.<sup>8</sup> Figure 3(b) shows the images of the near-field scattering amplitude over the same  $4 \times 4 \mu\text{m}^2$  area obtained by using a scattering scanning near-field infrared microscope operating at the infrared frequency of  $930 \text{ cm}^{-1}$ .<sup>8</sup>

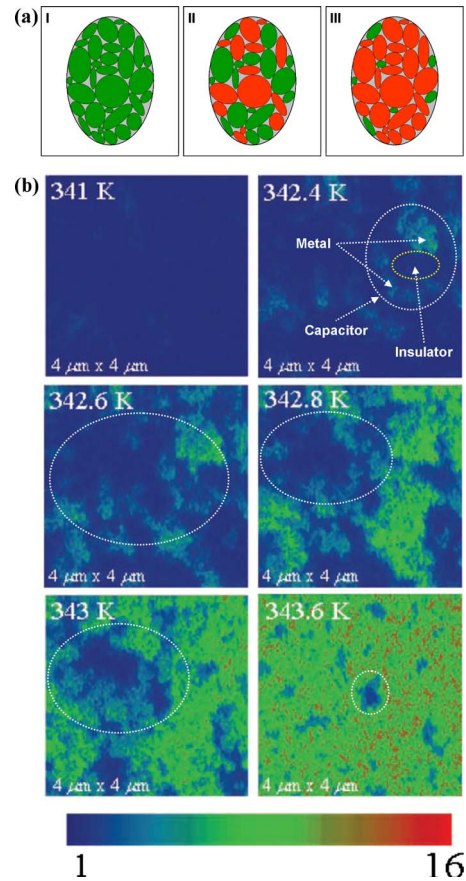


FIG. 3. (Color online) (a) An explanation on the formation of capacitance within the VO<sub>2</sub> device during the MIT. The green and red grains indicate the high and low resistance states (insulating and metallic states) of the VO<sub>2</sub> phase, respectively. The gray bottom is a non-VO<sub>2</sub> phase-like grain boundary. (b) Images of the near-field scattering amplitude over the same  $4 \times 4 \mu\text{m}^2$  area obtained by using a scattering scanning near-field infrared microscope operating at the infrared frequency  $\omega = 930 \text{ cm}^{-1}$ .

These images are displayed for representative temperatures (341.0, 342.4, 342.6, 342.8, 343.0, and 343.6 K) in the MIT regime of VO<sub>2</sub> and show the percolative nature of the MIT in progress. The metallic regions (green and red colors) give higher scattering near-field amplitude compared with the insulating phase (dark blue color), e.g., the region surrounded by the yellow dotted line in Fig. 3(b). These images directly show that the insulating and metallic phases coexist in VO<sub>2</sub> over a finite temperature range in the transition region. Thus, insulating and metallic phases in the region surrounded by the white dotted lines in Fig. 3(b) may act as dielectric components and metal electrodes, respectively, resulting in the formation of a capacitor across the device. Further experimental evidence for the construction and destruction of capacitance in VO<sub>2</sub> comes from observing the infrared resonance frequency of a hybrid-metamaterial comprised of splitting-resonators and VO<sub>2</sub>.<sup>57</sup>

## C. Applied voltage dependence of $f_{\text{osc}}$

In order to investigate the dependence of  $f_{\text{osc}}$  on applied voltage (for a fixed value of  $R_E$  with 1 k $\Omega$  step), the electrical responses of  $V_D$  and  $I_D$  were measured for increasing  $V_S^p$ . Among the measurement results, Figs. 4(a) and 4(b) show

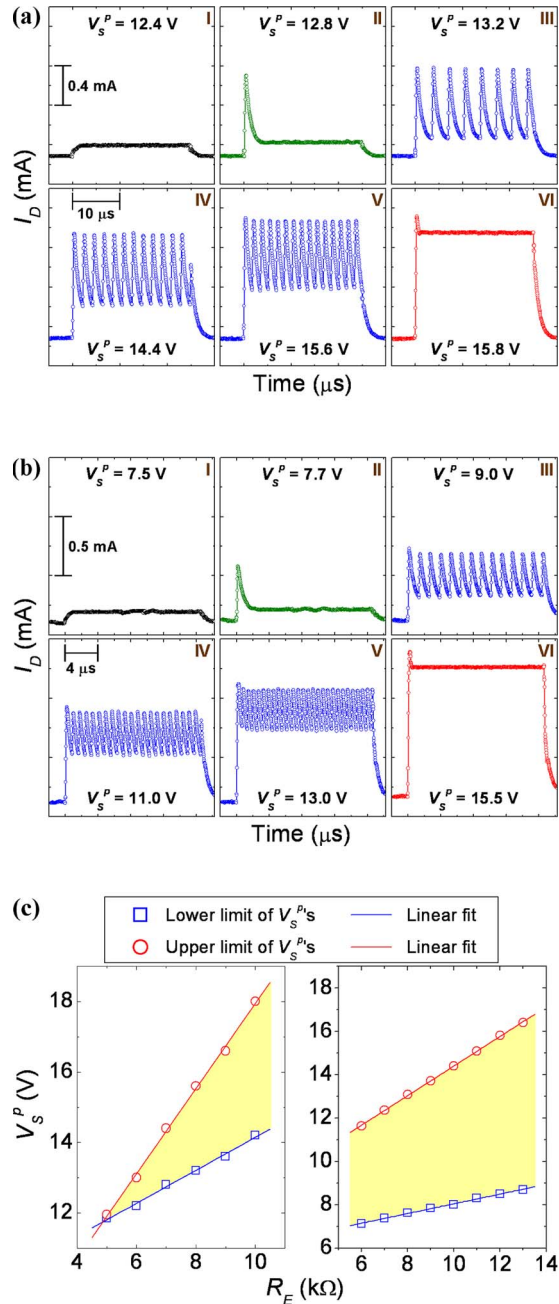


FIG. 4. (Color online) Life cycle of the MIT oscillation of  $I_D$  in (a) device I and (b) device II measured at  $R_E$  of 8 and 10 k $\Omega$  with respect to various values of  $V_S^p$ , respectively. (c) A generation window of the MIT oscillation. The lower and upper limits of  $V_S^p$  where the oscillation can be generated at each  $R_E$  are plotted with blue squares and red circles, respectively. The left and right subplots indicate the generation window of the MIT oscillation in device I and device II, respectively.

the life cycles of the MIT oscillation, measured in  $I_D$ , for device I and device II (measured at  $R_E$  of 8 and 10 k $\Omega$  with respect to various values of  $V_S^p$ ). In device I and device II,  $V_S^p$ 's in subplots I, II, III, IV, V, and VI correspond to 12.4, 12.8, 13.2, 14.4, 15.6, and 15.8 V and 7.5, 7.7, 9.0, 11.0, 13.0, and 15.5 V, respectively.

In plot I of Figs. 4(a) and 4(b), current pulses with peak values of  $\sim 0.40$  and  $\sim 0.19$  mA and pulse widths of 25 and  $\sim 16.67$   $\mu$ s are observed without any  $I_D$  oscillation. This implies that  $V_D$  does not reach  $V_{t1}$  yet. In plot II of Figs. 4(a)

and 4(b), current pulses with impulsive peaks whose values are  $\sim 1.10$  and  $\sim 0.58$  mA are observed, respectively, and the  $I_D$  oscillation is not yet observed. This is because  $V_S^p$  is not large enough to make  $V_D$  decreased after the MIT reach  $V_{t1}$ . In plots III, IV, and V of Figs. 4(a) and 4(b), periodical waveforms composed of impulsive peaks of  $I_D$  are observed, i.e., the  $I_D$  oscillation is observed. This suggests that  $V_S^p$  is large enough to make  $V_D$  decreased after the MIT reach  $V_{t1}$ . In these three plots (III, IV, and V), we observe that  $f_{osc}$  increases in proportion to  $V_S^p$ , and a detailed discussion on the relationship between  $f_{osc}$  and  $V_S^p$  will be provided in Sec. III D. In plot VI of Figs. 4(a) and 4(b), rectangular pulses with average values of  $\sim 1.35$  and  $\sim 1.26$  mA, respectively, emerge without the periodical waveform. This extinction of the MIT oscillation is caused by the collapse of the capacitive component of the device [disappearance of dark blue region in Fig. 3(b)] due to Joule heat generated by a large value of  $I_D$  induced by  $V_S^p$  increase.

In order to find a region of  $R_E$  and  $V_S$  within which the MIT oscillation can be generated, the oscillation characteristics of the VO<sub>2</sub> devices were measured with several values of  $R_E$  and  $V_S^p$ . A specific region of  $R_E$  and  $V_S^p$ , where the MIT oscillation is generated, can be determined in a two-dimensional domain defined with  $R_E$  and  $V_S^p$ , as shown in Fig. 4(c). The left and right subplots in Fig. 4(c) indicate the generation window of the MIT oscillation in device I and device II, respectively. The lower and upper limits of  $V_S^p$  where the MIT oscillation can be generated for each  $R_E$  are plotted with blue squares and red circles, respectively. The solid lines are linear fits of the lower and upper limits of  $V_S^p$ , and the yellow region enclosed by solid lines thus illustrates the generation window of the MIT oscillation for our two devices. This oscillation window can also be predicted from both relationships:  $V_D \geq V_{t1}$  and  $I_D \leq I_{t2}$ . The graphical intersection of these two one-dimensional inequalities with two variables ( $R_E$  and  $V_S^p$ ) creates a unique region in the two-dimensional domain of  $R_E$  and  $V_S^p$ . It can be verified from simple graphical analysis that this calculated region is in good agreement with the measured oscillation window [yellow region of Fig. 4(c)].

## D. Analysis of oscillation waveform

In order to further investigate the dependence of  $f_{osc}$  on  $V_S$ , oscillation waveforms of  $V_D$ , measured at  $R_E = 8$  k $\Omega$  for three values of  $V_S^p$  (13.8, 14.6, and 15.4 V), were superimposed, as shown in Fig. 5(a). As mentioned earlier, abrupt drops of  $V_D$  from points A, C, and E to points B, D, and F labeled in the figure are induced by the MIT of the VO<sub>2</sub> film. As seen from the figure, we can recognize two important features: the temporal intervals of traces A-B, C-D, and E-F labeled in the figure are nearly the same ( $\sim 0.36$   $\mu$ s) regardless of  $V_S^p$ . The time required for dropped  $V_D$  to recover to  $V_{t2}$  (by some elastic restoring force<sup>27</sup>) is also nearly the same ( $\sim 0.14$   $\mu$ s) regardless of  $V_S^p$  with respect to each trace B-B', D-D', and F-F'. Thus, the time consumed on the exponential growth of  $V_D$  from  $V_{t2}$  to  $V_{t1}$ , e.g.,  $t_1$  at  $V_S^p = 15.4$  V (or  $t_2$  and  $t_3$  at  $V_S^p = 14.6$  and 13.8 V, respectively), dominantly contrib-

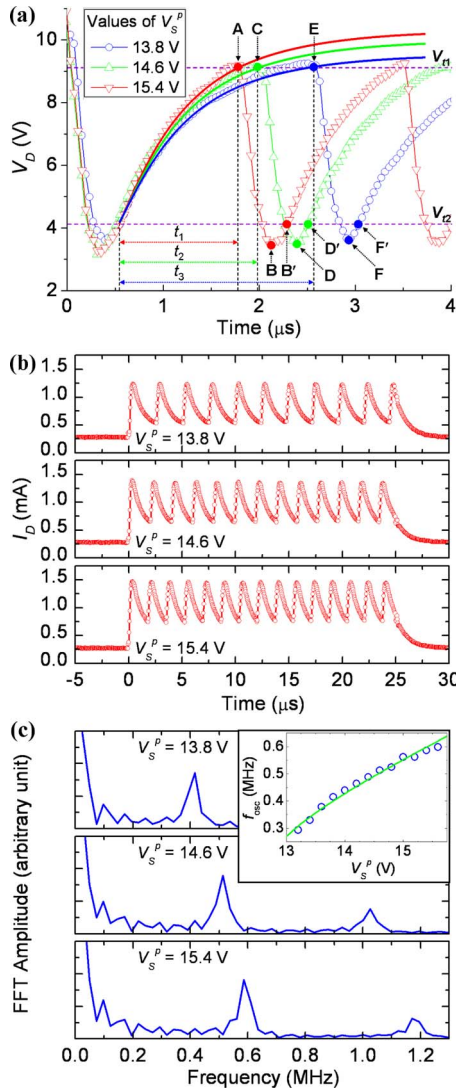


FIG. 5. (Color online) (a) Superimposed waveforms of  $V_D$  measured in device I serially connected with  $R_E = 8 \text{ k}\Omega$  with respect to three values of  $V_S^p$  (13.8, 14.6, and 15.4 V). (b) Measured waveforms of  $I_D$  oscillation. (c) Their FFT amplitude spectra with respect to various values of  $V_S^p$  (only three cases including 13.8, 14.6, and 15.4 V are displayed) at  $R_E = 8 \text{ k}\Omega$ , when the rectangular voltage pulse with a pulse width of  $25 \text{ }\mu\text{s}$  is applied to device I. The inset plot shows the functional relationship between  $f_{\text{osc}}$  and  $V_S^p$ .

utes to the determination of  $f_{\text{osc}}$ . We can fit this exponential growth section from  $V_{I2}$  to  $V_{I1}$  with the function

$$V_D(t) = (V_A - V_{I2})\{1 - \exp[-(t - t_0)/\tau_0]\} + V_{I2}. \quad (3)$$

This exponential buildup of  $V_D$  in Eq. (3) means the buildup of charge on the capacitor in a series RC circuit, which is predicted in Eq. (1). This means that  $\tau_0$  in Eq. (3) limiting the maximum  $f_{\text{osc}}$  is the same as that in Eq. (1), and  $\tau_0$  is proportional to  $C_D R_E$ .  $\tau_0$ 's of the fitting curves evaluated from the traces were  $\sim 0.840$ ,  $\sim 0.801$ , and  $\sim 0.765 \text{ }\mu\text{s}$  for  $V_S^p$ 's of 13.8, 14.6, and 15.4 V, respectively. This indicates that  $\tau_0$  decreases when  $V_S^p$  increases, i.e.,  $C_D$  decreases with the increase in  $V_S^p$ . When the effect of  $R_D$  dependent on  $V_S^p$  on  $\tau_0$  is ignored,  $C_D$  can easily be estimated as  $\sim 105.0$ ,  $\sim 100.1$ , and  $\sim 95.6 \text{ pF}$  (for  $V_S^p$ 's of 13.8, 14.6, and 15.4 V, respectively). When we postulate the circuit model of the VO<sub>2</sub> device as the parallel connection of  $C_D$  and  $R_D$ ,  $\tau_0$  is given as

$R_E C_D [R_D / (R_D + R_E)]$ , and thus  $C_D$  becomes larger in general cases compared with the above values ( $\sim 105.0$ ,  $\sim 100.1$ , and  $\sim 95.6 \text{ pF}$ ) and goes to the minimum in a special case such as  $R_D \rightarrow \infty$ , which is the same situation as the above case that  $\tau_0$  is independent of  $R_D$ . In addition to the relationship between  $\tau_0$  and  $V_S^p$ , the asymptotic voltage  $V_A$  in Eq. (3) also increases with  $V_S^p$ . As  $V_S^p$  increases, therefore, the exponential curve of  $V_D$  in Eq. (3) will be expanded due to the increase in  $V_A$ , as shown in red, green, and blue solid lines of Fig. 5(a). This will give rise to a faster arrival of  $V_D$  at  $V_{I1}$ , resulting in higher  $f_{\text{osc}}$ .

Figures 5(b) and 5(c) show the waveforms of  $I_D$  oscillation and their fast Fourier transform (FFT) amplitude spectra measured with respect to various  $V_S^p$ 's at  $R_E = 8 \text{ k}\Omega$  (only three cases including  $V_S^p$ 's of 13.8, 14.6, and 15.4 V are displayed), respectively, when the rectangular voltage pulse is applied to device I with a pulse width of  $25 \text{ }\mu\text{s}$ . The inset plot in Fig. 5(c) shows the functional relationship between  $f_{\text{osc}}$  and  $V_S^p$ , and the blue circles indicate the measured values of  $f_{\text{osc}}$  with respect to the various values of  $V_S^p$ . The green solid line indicates the curve fitted by a logarithmic function determining  $f_{\text{osc}}$  with respect to  $V_S^p$ , which is obtained by manipulating Eq. (3) in consideration of the oscillation period. It is observed that the curve initially shows a logarithmic response but asymptotically shows a linear response after  $V_S^p$  exceeds 14 V. In an approximately linear region, the tuning sensitivity, defined as  $(\Delta f_{\text{osc}} / \Delta V_S^p)$ , was calculated as  $99.18 \text{ kHz/V}$ . These results suggest that the VO<sub>2</sub> device can be utilized as a voltage-controlled oscillator, which consists of only two circuit components and is operated by only one voltage source.

## E. Effect of external parameters

We now consider controlling  $f_{\text{osc}}$  using passive external circuit components.  $f_{\text{osc}}$  is determined by  $1/(T_0 + T_1)$ , where  $T_0$  and  $T_1$  indicate the time required for  $V_D$  to increase from  $V_{I2}$  to  $V_{I1}$  and required for  $V_D$  to drop from  $V_{I1}$  to  $V_{I2}$ , respectively.  $f_{\text{osc}}$  is mainly dependent on  $T_0 = \tau_0 \ln(1 + [V_{I1} - V_{I2}] / [V_A - V_{I1}])$ , which is obtained by Eq. (3), because  $T_1$  is nearly the same ( $\sim 0.50 \text{ }\mu\text{s}$ ) regardless of  $V_S^p$ .  $T_0$  depends not only on  $V_S^p$  but also on  $\tau_0$ . This means that  $f_{\text{osc}}$  can be tuned by varying an external circuit parameter such as  $R_E$ . Also, when an external capacitor of a capacitance  $C_E$  is connected in parallel with the external resistor, as shown in the dashed box of Fig. 2(a), it becomes another  $f_{\text{osc}}$  tuning parameter because  $\tau_0$  is proportional to  $(C_E + C_D)R_E$ .

Based on the above discussion, external control of  $f_{\text{osc}}$  was demonstrated through the adjustment of  $R_E$  without external capacitor and the adjustment of  $C_E$  with  $R_E$  fixed ( $10 \text{ k}\Omega$ ). This experiment was done in device II, which was especially designed to obtain an enhanced frequency response. This frequency improvement is achieved because the reduced dimension of the VO<sub>2</sub> patch in device II reduces  $(V_{I1} - V_{I2})$ , but with  $C_D$  maintained as nearly the same value as that of device I. Thus,  $T_0$  and  $f_{\text{osc}}$  in device II become smaller and larger compared with those in device I, respectively.

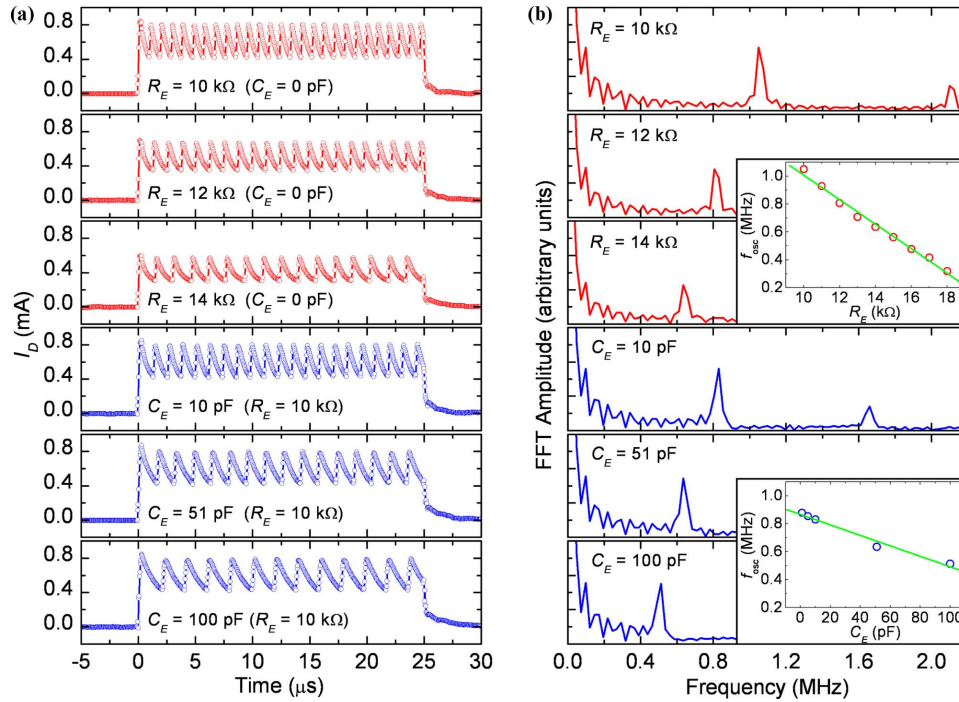


FIG. 6. (Color online) (a) Measured waveforms of  $I_D$  oscillation with respect to various external resistances (only three cases including  $R_E$ 's of 10, 12, and 14 k $\Omega$  at  $C_E=0$  are displayed) and various external capacitances (only three cases including  $C_E$ 's of 10, 51, and 100 pF at  $R_E=10$  k $\Omega$  are displayed), when the rectangular voltage pulse is applied to device II with  $V_S^p$  of 10 V (no dc offset) and a pulse width of 25  $\mu$ s. (b) FFT amplitude spectra of  $I_D$  oscillation, as shown in Fig. 5(a), measured with respect to various external resistances and capacitances. The upper and lower inset plots show the linearity of the measured values of  $f_{osc}$  with respect to  $R_E$  and  $C_E$ , respectively.

Figure 6(a) shows the measured waveforms of the  $I_D$  oscillation with respect to various external resistances (three cases  $R_E=10$ , 12, and 14 k $\Omega$  at  $C_E=0$  are displayed) and various external capacitances (three cases  $C_E=10$ , 51, and 100 pF at  $R_E=10$  k $\Omega$  are displayed). As before, a rectangular voltage pulse is applied with  $V_S^p$  of 10 V (no dc offset) and a pulse width of 25  $\mu$ s. Figure 6(b) shows the FFT amplitude spectra of the corresponding  $I_D$  oscillation shown in Fig. 6(a).

From the figure, it is clearly observed that  $f_{osc}$  decreases with increasing  $R_E$  and  $C_E$ . A remarkable difference is that the mean value of the peak current and peak-to-peak amplitude have relatively strong dependence on  $R_E$  compared with that on  $C_E$ . This is caused by the fact that the amplitude of  $I_D$  includes a term of  $(V_S R_D / R_E)$  directly affected by  $R_E$ . The upper and lower inset plots of Fig. 6(b) show the linearity of the measured values of  $f_{osc}$  with respect to  $R_E$  and  $C_E$ , respectively. In each inset, the circular points indicate the measured values of  $f_{osc}$  with respect to  $R_E$  or  $C_E$ , and the solid lines indicate their linear fits. The tuning sensitivities, defined as  $(\Delta f_{osc} / \Delta R_E)$  and  $(\Delta f_{osc} / \Delta C_E)$ , were calculated as 87.89 kHz/k $\Omega$  and 3.76 kHz/pF, respectively. The standard deviations of the linear fits in upper and lower insets were calculated as 0.0267 and 0.0282, respectively. These results suggest that a VO<sub>2</sub> two-terminal device can be incorporated as a simple oscillator whose frequency is tuned by only passive circuit components such as resistors and capacitors. In addition, the sensitivity of  $f_{osc}$  on  $V_S^p$  makes this device a good candidate for a voltage-controlled oscillator. Previous experimental evidence that light can photoinduce the MIT transition in VO<sub>2</sub> suggests that this is another possible external control parameter for these oscillations.

## IV. COMPARISON ANALYSIS OF MOTT MIT AND PEIERLS (CDW) MIT

### A. The Mott MIT as evidenced by the observed current jump

The observed MIT-driven electrical oscillation occurs between instabilities  $P_1(V_{t1}, I_{t1})$  and  $P_2(V_{t2}, I_{t2})$  at the  $I$ -mode trace, and begins at  $P_1$  in Figs. 1(c) and 1(d). Since  $I$ -mode limits a current flow, the jump appears as a jump in voltage instead of a current jump. This jump has a very small hysteresis, as shown in Figs. 1(c) and 1(d). The small hysteresis indicates that the generated heat is small and does not reach the temperature needed to induce a SPT. This was directly proved by simultaneous measurements of micro-x-ray diffraction and  $I$ - $V$  measurements.<sup>31</sup> The current jump in the  $V$ -mode trace in Figs. 1(c) and 1(d), viewed as the MIT, is thus independent of any SPT.<sup>32</sup> A jump in resistance not accompanied by a SPT was also revealed by observing the temperature dependence of coherent phonons<sup>30</sup> and the pressure dependence of phonons.<sup>26–28</sup> It was also disclosed that current jump near the SPT temperature disappears.<sup>5,35</sup> Hole carriers were observed at the semiconductor side near 67 °C.<sup>5,9</sup>

As shown in plot VI's of Figs. 4(a) and 4(b), heat generation caused by an increase in current through our device makes the MIT-driven electrical oscillation disappear. The available experimental results draw a decision that the electrical oscillation does not occur above a certain high temperature. It is deduced that this oscillation is below 77 °C<sup>30</sup> based on the experimental results.<sup>5,26–28,30–32</sup> Thus, the microscopic physics responsible for inducing the observed electrical oscillation is that of the hole-driven Mott MIT.<sup>1,3,4</sup>



## B. The MIT analysis in view of CDW

Since it has been suggested that the MIT oscillation is related to CDW or charge ordering for  $K_{0.3}MoO_3$  and an organic material,<sup>48,49</sup> we discuss the MIT in view of the CDW. CDW (or charge ordering) is a charge imbalance between nearest-neighbor sites. In order to understand charge ordering of CDW, we introduce the Holstein CDW potential energy in the context of the Peierls MIT.<sup>13</sup> The CDW energy is given by  $V_{CDW} = -(b^2/k)(q_i - q_j)^2$  at  $x_o = (b/k)(q_i - q_j)$ , where  $b$  is a damping coefficient produced by charge difference between nearest-neighbor sites ( $i$  and  $j$  sites) of  $\Delta q = (q_i - q_j)$ ,  $k$  is the spring constant of an oxygen atom,  $(b^2/k)$  is the strength of electron-phonon interaction, and  $x_o$  is a distortion length of a lattice from an equilibrium position. As an example of CDW,<sup>13</sup> when we set two electrons at site  $i$  and no electron at the nearest-neighbor site  $j$ , the charge ordering (or charge difference) between nearest-neighbor sites is  $\Delta q \equiv (q_i - q_j) = (2 - 0) = 2$ .

The melting of charge ordering indicates the Peierls MIT where  $V_{CDW}$  and  $x_o$  approach zero due to  $\Delta q \rightarrow 0$ . This suggests that the distortion of the structure continuously lessens and finally disappears. Further, the Peierls CDW MIT should exponentially occur with carrier doping or temperature.<sup>13</sup> The sliding of the CDW is for  $\Delta q$  bound by  $V_{CDW}$  to tunnel to the nearest-neighbor site. Therefore,  $\Delta q$  is not observed in conduction band by Hall effect measurement. However, since the carriers used for the MIT oscillation are the ones of the conduction band, the tunneling bound charges in  $V_{CDW}$  are not used as an electrode. Moreover, the  $M_2$  phase of  $VO_2$  has both charge ordering and a Mott Hubbard insulator; one-half of the V chain pairs but does not twist (this forms charge ordering of CDW) and the other half twists but does not pair (this is an equally spaced V zigzag chain and forms the Mott-Hubbard insulator).<sup>17,18</sup> Thus, since it has been known that the first-order MIT in  $VO_2$  comes from the equally spaced V chain,<sup>18,30</sup> and that the SPT is continuous,<sup>30</sup> we suggest that the abrupt MIT cannot be explained in terms of the Peierls (CDW) MIT. Note that it can be right that the MIT oscillation is based on the CDW theory for materials following characteristics of CDW such as  $K_{0.3}MoO_3$ <sup>48</sup> and an organic material.<sup>49,50</sup>

## V. CONCLUSION

In conclusion, we have demonstrated sustained electrical oscillations in a simple series circuit comprised of a voltage source, a resistor, and our  $VO_2$  device. These oscillations are the result of the MIT in  $VO_2$ . It is shown that these MIT oscillations are attributed to the creation and destruction of a capacitor composed of the semiconducting and metal phases of  $VO_2$ . These two phases—coexisting at a nanoscale in  $VO_2$  during the MIT—can be regarded as the dielectric material and electrodes of many nanocapacitors. Since these capacitive components disappear with input heat energy, the MIT oscillation is best explained not in terms of Joule heating inducing a SPT but in terms of hole carriers (or electronic carriers) driving a Mott MIT. Thus, the presence of the MIT oscillation in the  $VO_2$  devices becomes the evidence of the Mott MIT.

Furthermore, the qualitative and quantitative analyses of experimental results suggest that this MIT oscillation, whose frequency can be tuned by active or passive circuit components, can be beneficially applied to fields of power electronics including inverters, high-voltage dc transmission systems, and static synchronous compensators.<sup>58</sup>

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